

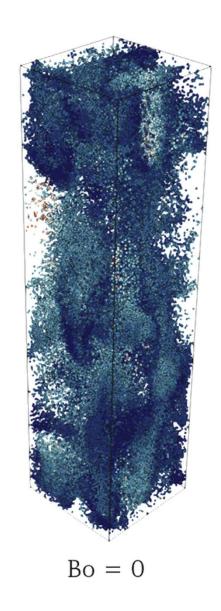
Beyond classical CFD-DEM

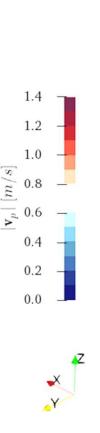
Forgotten Challenges and New Tools S. RADL

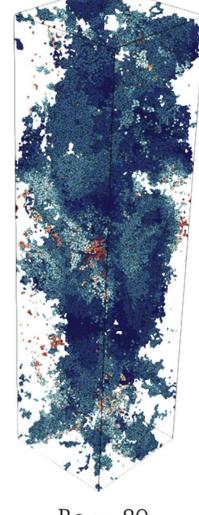
with contributions from M. ASKARISHAHI, H. BENABCHIASLI, N. GHODS, F. GOIO CASTRO, M. SALEHI, S. SUNDARESAN, & J. TAUSENDSCHÖN

SFB/CRC 287 Retreat

June 13, 2023 Hannover

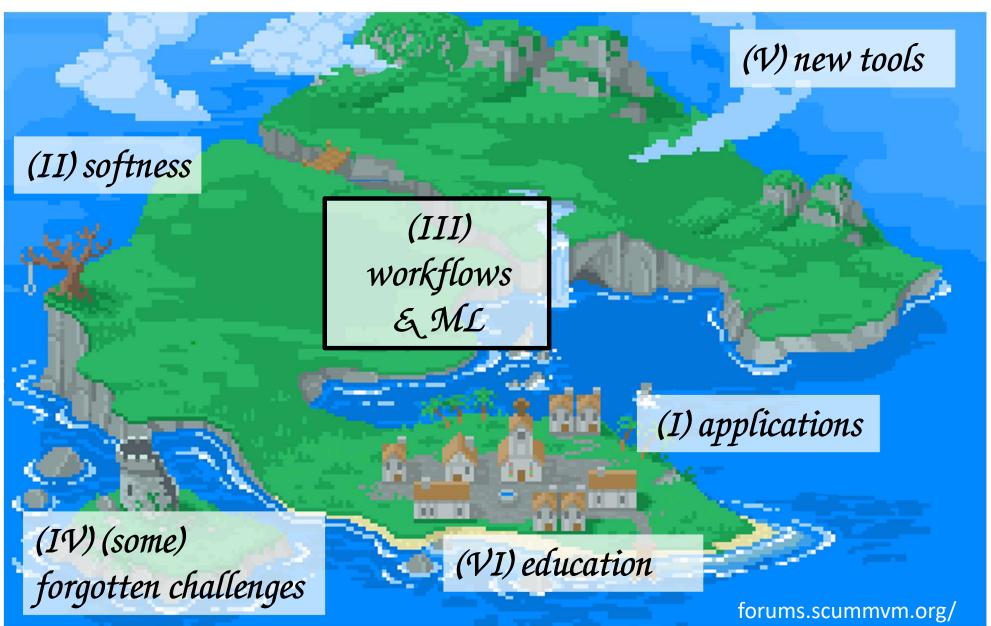






Overview







Graz University of Technology

Batteries I: thermal runaway

...super fast, super hot and supersonic

...tribocharging

...hydrolysis of water vapor

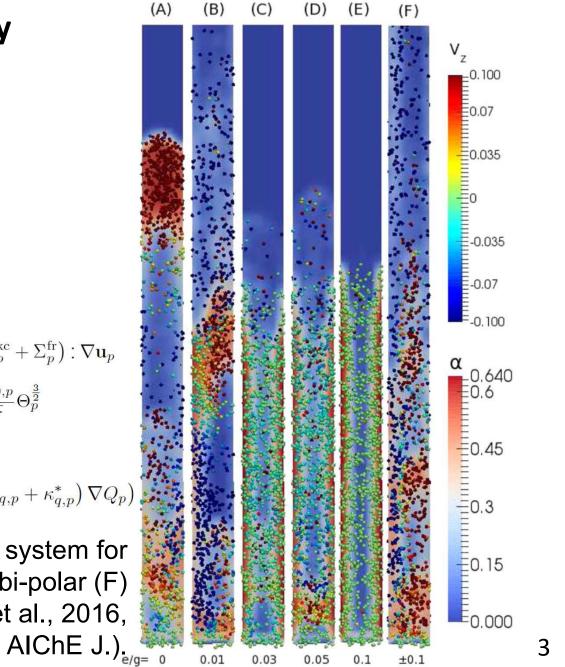
...sparks and arcs

...800V operating voltage

$$\frac{3}{2} \frac{\partial}{\partial t} \left(\alpha_p \rho_p \Theta_p \right) + \frac{3}{2} \nabla \cdot \left(\alpha_p \rho_p \Theta_p \mathbf{u}_p \right) = \nabla \cdot \left(\kappa_p \nabla \Theta_p \right) - \left(\Sigma_p^{\text{kc}} + \Sigma_p^{\text{fr}} \right) : \nabla \mathbf{u}_p \\
- 12 \left(1 - e_{c,p}^2 \right) \frac{\alpha_p^2 \rho_p g_{0,p}}{d_p \sqrt{\pi}} \Theta_p^{\frac{3}{2}} \\
- 3\beta \Theta_p,$$

$$\frac{\partial}{\partial t} \left(\frac{\alpha_p}{V_p} Q_p \right) + \nabla \cdot \left(\frac{\alpha_p}{V_p} Q_p \mathbf{u}_p \right) = \nabla \cdot (\sigma_{q,p} \mathbf{E}) + \nabla \cdot \left(\left(\kappa_{q,p} + \kappa_{q,p}^* \right) \nabla Q_p \right)$$

Behavior of a fluidized gas-particle system for uncharged (A), monopolar (B-E), and bi-polar (F) particle charging (Kolehmainen et al., 2016,



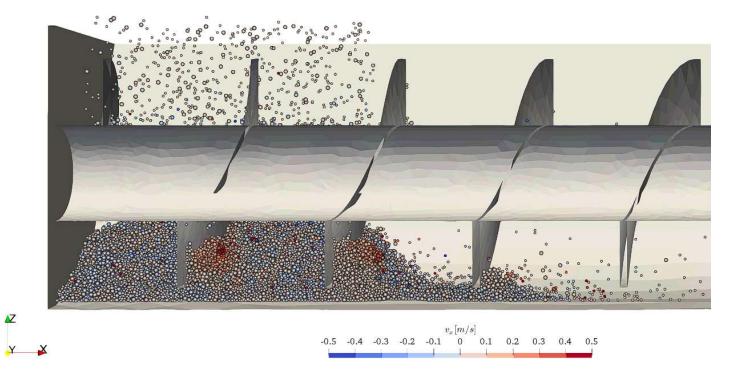


Batteries II: recycling

...keep cool! (because of reactions)

...really complex rheology (wet fibres mixed with small particles) \rightarrow calibration

...spontaneous carbonation in air (changing rheology)



Cohesive battery recyclate flow in a screw conveyor (Hadie Benabchiasli)

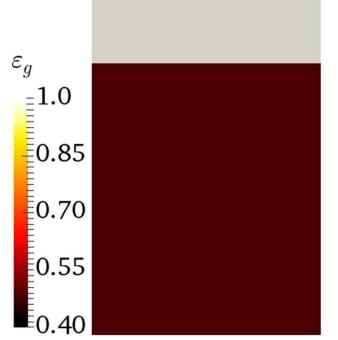


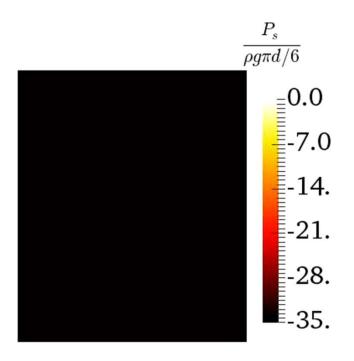
Wet Granulation

...fluidization of cohesive powders

... spraying & drying

... binders with complex rheology





Askarishahi et al., Processes, 2023

Askarishahi et al., Ind. Eng. Chem. Res. 61, 2022

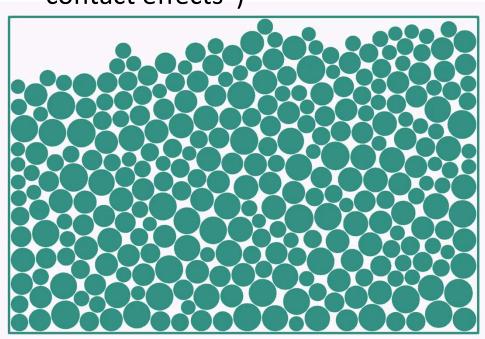


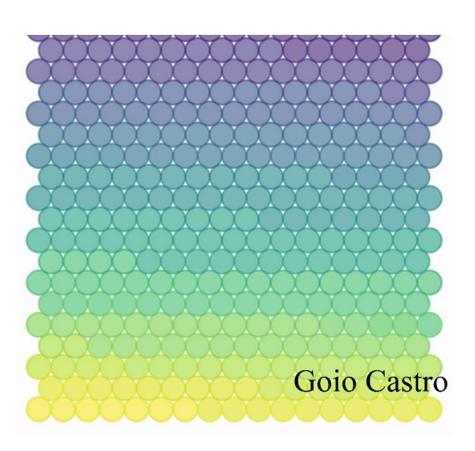
Compaction and discharge

...unsteady gas-particle at extreme speed (bag filling time < 1 s)

...effect of (relative) softness

...multi-contact DEM model ("neighbor contact effects")

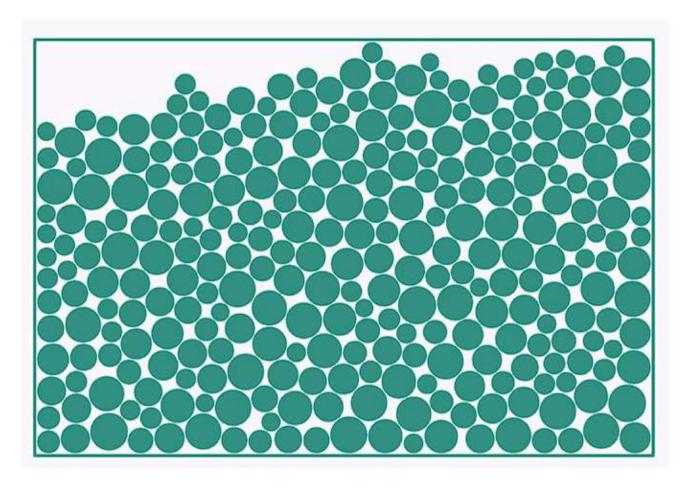


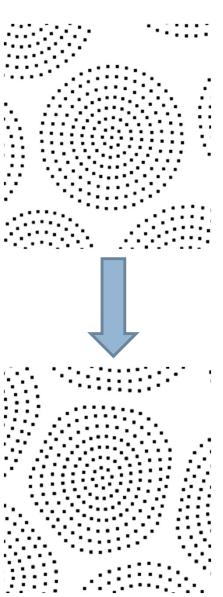


SPH-DEM simulation of compaction (left) and silo discharge (right; 2D Francisco Goio Castro)



 Approach I: Resolved Particles with SPH-DEM



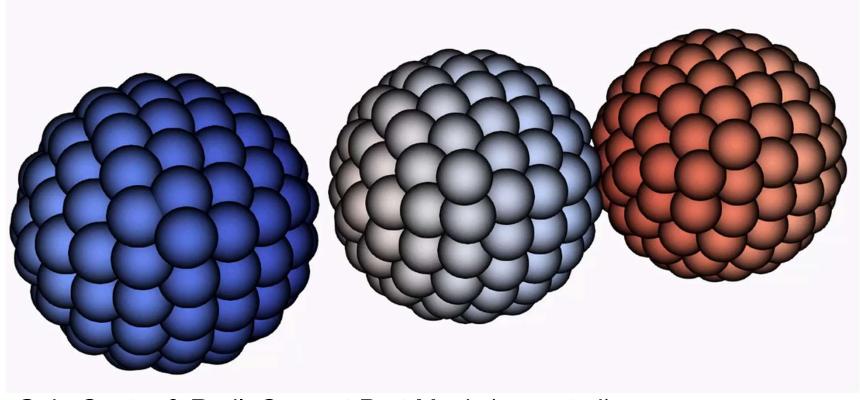


Goio Castro & Radl, Comput Part Mech (accepted)



Approach I: Resolved Particles with SPH-DEM

- ...SPH for intra-particle deformation
- ...DEM-type model for inter-particle interactions (penalty approach)



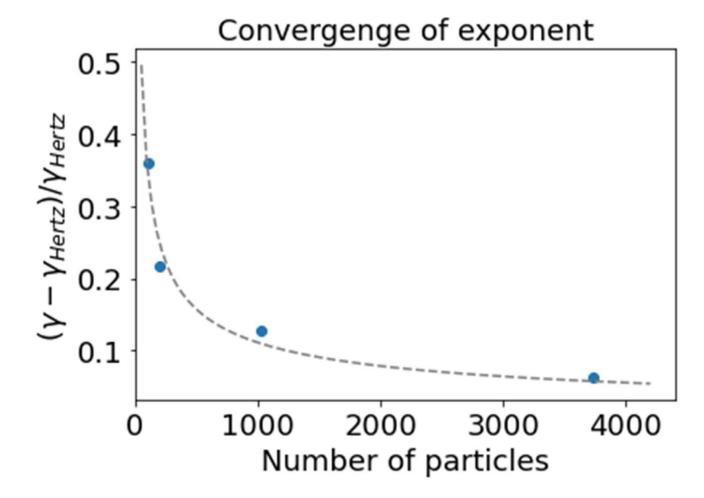
Goio Castro & Radl, Comput Part Mech (accepted)



Approach I: Resolved Particles with

SPH-DEM

Resolution Requirements: force Exponent in overlap relation: $F_{con}t \propto \delta^{\gamma}$





Approach II: Multi-Contact (MC) Force Closure

Basics and Benchmarking (Compaction)

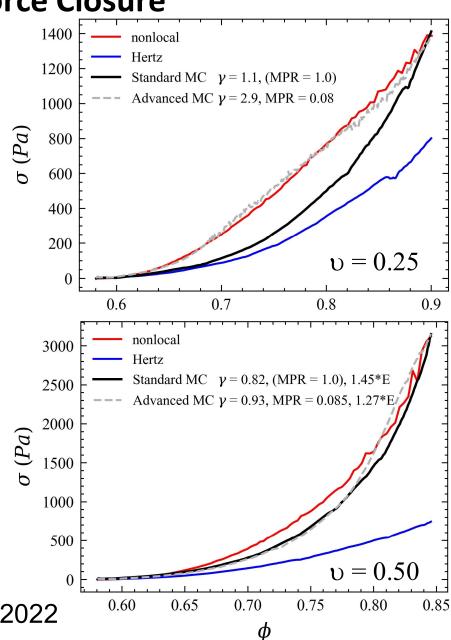
$$\delta_c = (r_i + r_j) - (\mathbf{x}_i - \mathbf{x}_j) \cdot \mathbf{n}$$

$$\delta_{k \to c}$$

$$= -\gamma \frac{(1+\upsilon)F_k}{2\pi E d_{kc}} \left\{ (\mathbf{n}_k \cdot \mathbf{u}_{kc})(\mathbf{n}_c \cdot \mathbf{u}_{kc}) + (3 + \varepsilon) \right\}$$

$$-4\upsilon)\mathbf{n}_{k}\cdot\mathbf{n}_{c}-(1-2\upsilon)\frac{(\mathbf{n}_{k}+\mathbf{u}_{kc})\cdot\mathbf{n}_{c}}{1+\mathbf{n}_{k}\cdot\mathbf{u}_{kc}}\bigg\} \stackrel{\widehat{\mathbf{g}}}{\overset{\widehat{\mathbf{g}}}}{\overset{\widehat{\mathbf{g}}}{\overset{\widehat{\mathbf{g}}}}{\overset{\widehat{\mathbf{g}}}}{\overset{\widehat{\mathbf{g}}}{\overset{\widehat{\mathbf{g}}}}}{\overset{\widehat{\mathbf{g}}}}}{\overset{\widehat{\mathbf{g}}}}{\overset{\widehat{\mathbf{g}}}}}{\overset{\widehat{\mathbf{g}}}}}{\overset{\widehat{\mathbf{g}}}}{\overset{\widehat{\mathbf{g}}}}{\overset{\widehat{\mathbf{g}}}}}}{\overset{\widehat{\mathbf{g}}}}{\overset{\widehat{\mathbf{g}}}}}{\overset{\widehat{\mathbf{g}}}}}}}}}}}}}}}}}}}}}$$





Ghods et al., Powder Technol., 2022



Approach II: Multi-Contact (MC) Force Closure

 10^{-1} Application case: dense shear $\phi = 0.625$ flow (Lees-Edwards BCs) $\phi = 0.650$ $\phi = 0.700$ ₹ 10⁻² $\phi = 0.750$ $\phi = 0.800$ $\phi = 0.850$ $\phi = 0.900$ 10^{-3} v = 0.3 10^{-5} 10^{-3} 10^{-2} 10^{-4} 10^{-1} $\phi = 0.625$ $\phi = 0.650$ $\phi = 0.700$ ₹ 10⁻² $\phi = 0.750$ $\phi = 0.800$ $\phi = 0.850$ 10^{-3} v = 0.5

 10^{-5}

 10^{-4}

 10^{-3}

 $\hat{\dot{\gamma}} \equiv \dot{\gamma} d/\sqrt{k/\rho}$

 10^{-2}

Overview





Workflows & ML



From the past...

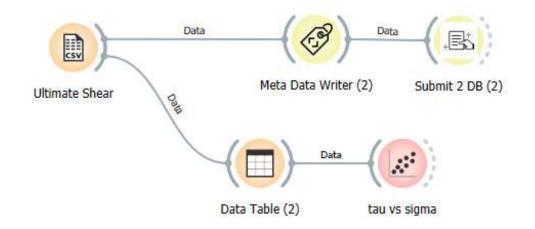
..."New" NNs

...via coarse graining

...to anisotropic drag corrections

...via the Need 4 Speed...

...to new perspectives

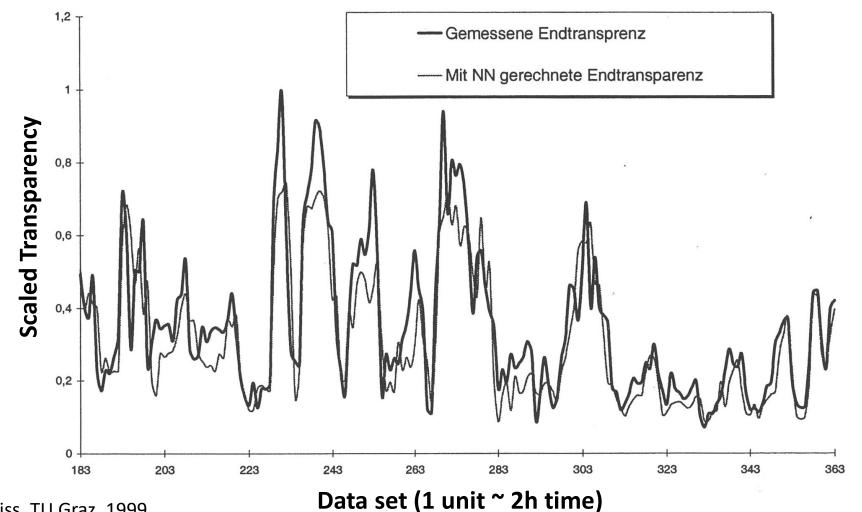






- "SNNS" is created in 90's as a tool to make predictions
- Fuchs uses SNNS to predict sedimentation performance of sludge based on training with 182 (!) data points

"Smart" (ML-based) predictors

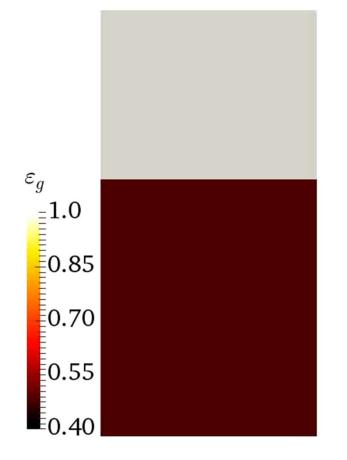


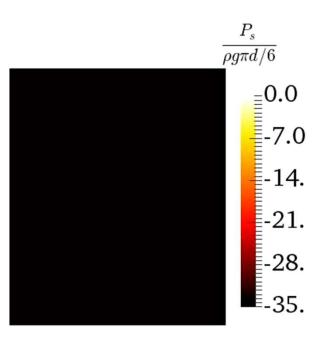


The **need for coarse graining** when simulating suspensions is demonstrated (Agrawal et al, 2001; Radl & Sundaresan, 2014)

Euler-Euler, and Euler-Lagrange simulators

 Refinement of E-L and E-E simulators and post-processing tools (Capecelatro & Desjardins, 2013)





Askarishahi et al., Ind. Eng. Chem. Res., 61, 2022.

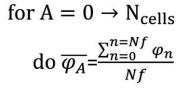


Tools

Dedicated tools for spatial averaging were developed

(Municchi et al., 2016)

"Filtering" (averaging)



endfor

No final step required

 φ : field to be filtered

A: current filtered cell

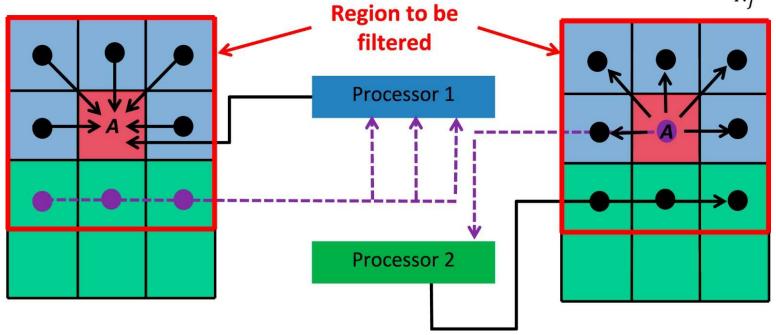
n: neighboring cells

for $A = 0 \rightarrow N_{cells}$

do
$$\varphi_n += \varphi_A$$

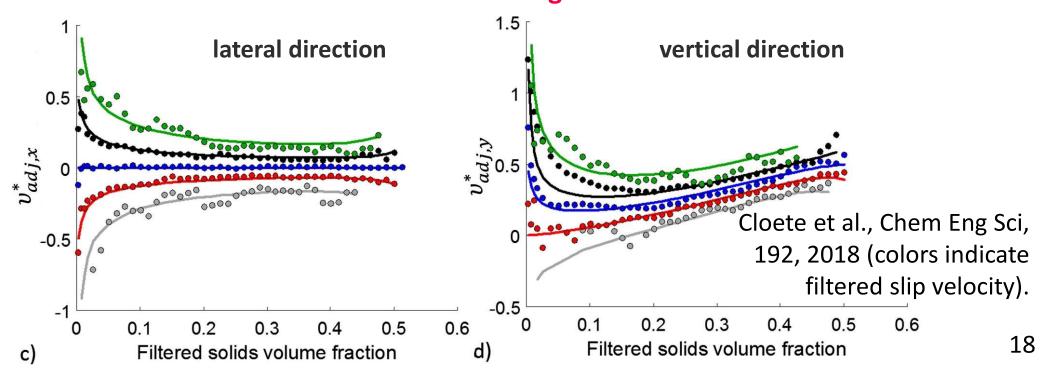
endfor

Final step:
$$\overline{\varphi_n} = \frac{\varphi_n}{N_f}$$





- New families of closure strategies were developed ("refiltering" idea of Schneiderbauer and Saeedipour, PoF, 30, 2018)
 - filtered TFM, "fast" CFD, novel closures
- ...or modeling is entirely data-driven ("rCFD play back" approach of Lichtenegger and Pirker, Chem Eng Sci, 153, 2016).
- Anisotropy of corrections is (not surprisingly!) identified as a key need. This is relevant for stress and drag terms!



Workflows & ML::Need4Speed



Particles which are fine or with cohesive interactions (e.g., liquid

bridge force) are widely used

Pharmaceuticals







Food



- Challenges
- agglomeration and segregation
- blockage & depositions
- inefficient mixing
- Equipment performance <20%

- Experimental route
- Expensive, difficult & dirty
- o indirect & noisy data from the plant

https://www.gea.com/en/

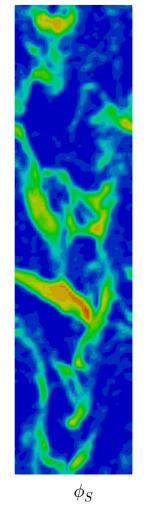
https://burnertec.com/fcc-equipments/

https://www.industrialmeeting.club/food-processing-industry-plant-for-dry-mixed-products/

Workflows & ML::Need4Speed



- Modeling of gas-particle flows in industrial-sized fluidized beds
 - Typically, coarse-grid simulations using a "filtered" two-fluid model (fTFM)
- fTFMs need sub-grid closure models to approximate unresolved physical phenomena
 - Account for the effects of the inhomogeneous particle distribution
 - The drag force is essential for reliable prediction of flow behavior
- Complexity increases when considering cohesive gas-particle flows
 - Cohesive influence on the filtered drag force closure
 - Need for faster (automated) closure development



0.00 0.20 0.40

0.65

Workflows & ML::Need4Speed::Model I

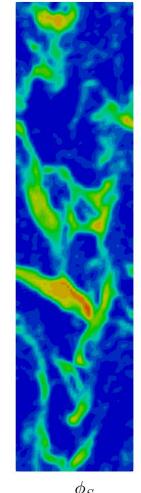


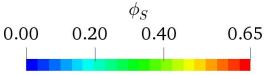
- Performing and then filtering of "fine grid" simulations
 - Euler-Euler Approach
 - Fluid and solid phase motion via continuum ansatz
 - complex particle-particle interactions (cohesion) challenging,
 but possible. However, not the current focus...

Euler-Lagrange Approach

- Classical continuum-based ansatz only for fluid phase
- Individual particle motion via Newton's equation of motion
- Large variety of models for particle-particle interactions
- ✓ Our current focus

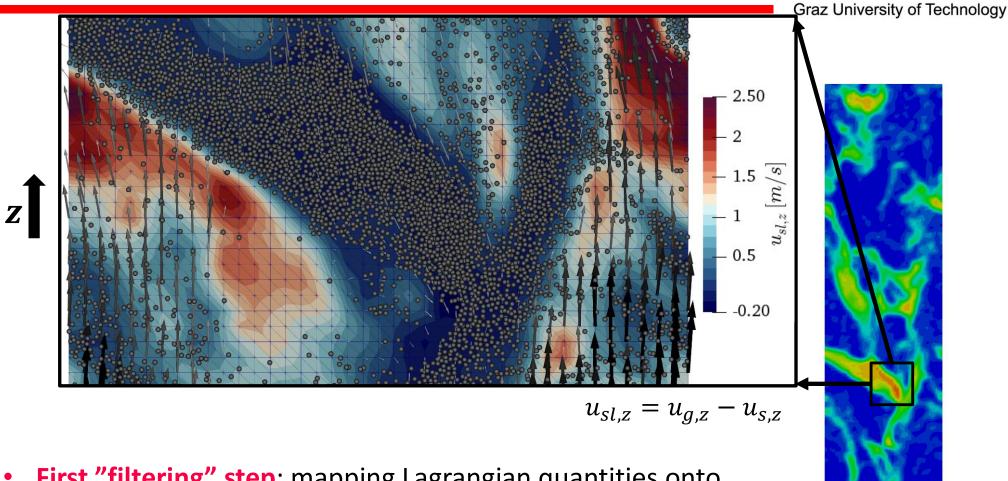
"ML-empowered" closure development



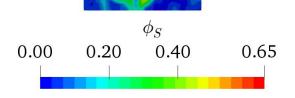


Workflows & ML::Need4Speed::Model II





- First "filtering" step: mapping Lagrangian quantities onto the fine Eulerian grid
- Second filtering step: Filter all relevant quantities using a defined filter length $\rightarrow \overline{\phi}_{S}$, \widetilde{u}_{q} , \widetilde{u}_{S}



Workflows & ML::Need4Speed::Model III



- Correction tensor $H_d = \frac{drag \ in \ inhomogeneous \ state}{drag \ in \ hypothetical \ homogeneous \ state}$
- This means it must fulfill the following properties:
 - \circ $H_d \rightarrow 1$ for sufficiently small filter sizes (i.e., "well-resolved" simulations)
 - \circ $H_d \rightarrow 1$ in the dilute limit (i.e., a single particle sedimenting at its terminal speed)
 - $0 H_d \rightarrow 1$ in the dense limit (i.e., a particle suspension sedimenting at steady state)
- **Previous approach**: correlation functions based on just few features ("markers"): $\bar{\phi}_s$, Δ_f , \tilde{u}_{sl} :
 - Complex to build, limited applicability (poor training, not rigorous)
 - limited accuracy for larger filter lengths
- Novel approach: usage of neural networks
 - Fast, accurate & rigorous (many markers), and easy to integrate (e.g., Keras2CPP)
 - previously only applied to dry systems

Workflows & ML::Need4Speed::Model Details

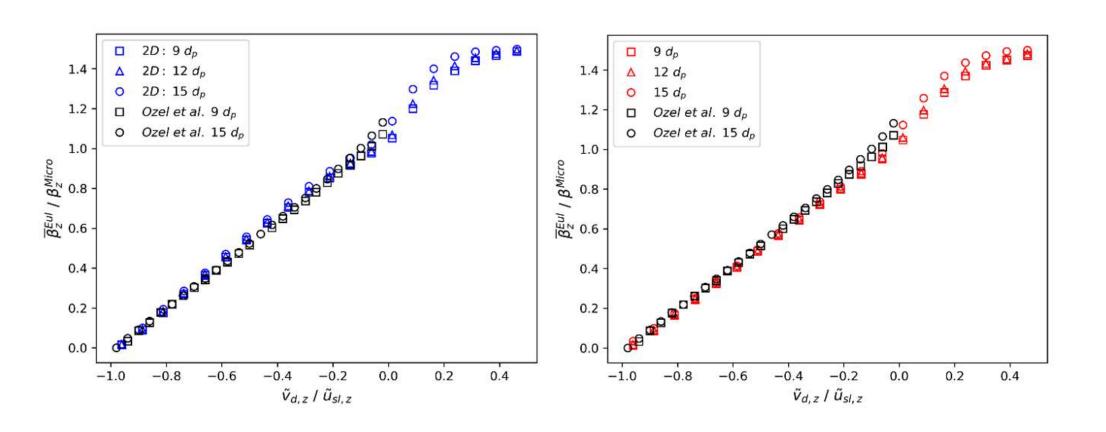


- Keras[®] framework in Python
- DNNs with three hidden layers are optimal
- Rectifying Linear Unit (ReLU) activation function
- Training: mini-batch gradient descent method (MB size: 1024), Mean Absolute Error (MAE) is the cost function
- Training time: 2D with 25 epochs → 0.5 hours, 3D with 50 epochs → 3.5 hours
- Hyperparameter search: up to 80 hrs in 3D

Workflows & ML::Need4Speed::Validation



"Validation" with previous work



Workflows & ML::Need4Speed::Result I



- Ansatz for the filtered drag force: $\overline{m{\Phi}}_{d,A} = m{H}_d \; eta^{Micro} \; \widetilde{m{u}}_{sl}$
- ...with the closure

$$\boldsymbol{H}_d = \mathbf{1} + \frac{\phi_{s,max} \, u_t}{\overline{\phi}_s \, \tilde{u}_{sl,z}} \boldsymbol{z}$$

The target and the prediction of the neural network is the scaled drift velocity

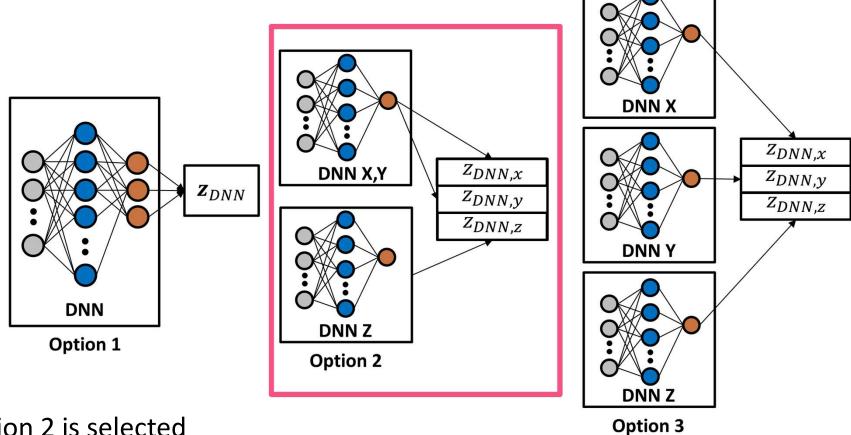
$$\mathbf{z} = \frac{\overline{\phi}_{S} \, \widetilde{\mathbf{v}}_{d}}{\phi_{S,max} \, u_{t}}$$

• For now, we consider all off-diagonal ("lift like") values of H_d to be zero. However, diagonal elements of H_d are not identical (anisotropic correction)

Workflows & ML::Need4Speed::Result II



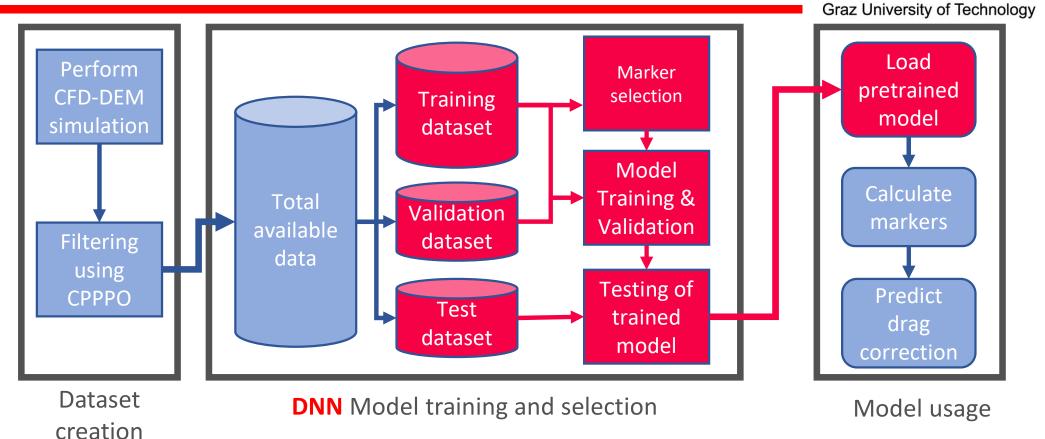
- Prediction based on vector-valued markers must ensure Galilean invariance
- Three basic options to formulate a drag correction



- Option 2 is selected
 - An internal coordinate system, that respects rotational invariance, can be intuitively spanned

Workflows & ML::Need4Speed::Result III





Markers ("Features")

$$\boldsymbol{\psi} = \left(\frac{1}{\Delta_f^*}, \frac{\overline{\phi}_S}{\phi_{S,max}}, \frac{\widetilde{\boldsymbol{u}}_{Sl}}{u_t}, \overline{\nabla p_Z^*}, Bo, \overline{\dot{\gamma}_{Sl}^*}, \overline{\dot{\gamma}_S^*}, \frac{\|\widetilde{\boldsymbol{u}}_{Sl,xy}\|}{u_t}\right)$$

All markers min/max normalized prior to usage

Workflows & ML::Need4Speed::Result IV



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$$\alpha = 3$$

- Pseudo 2D & 3D CFD-DEM simulations
 - Domain size is $16 \Delta_G \times 2 (or 16) \Delta_G \times 64 \Delta_G$
 - Total particle volume fraction $\phi_{s,tot}$ = 0.10
 - Filter sizes are: $3 \Delta_G$, $4 \Delta_G$, $5 \Delta_G$
- Scaling of coarse graining parameters following
 Tausendschön et al.
- Dry to highly cohesive systems (cohesion from liquid bridges: capillary & viscous)

	$\alpha = 3$
$d_P [\mu m]$	450
$\Delta_G [\mu m]$	1,350
N_{prime}	285,147
Parcels	10,561
<u> </u>	0 - 80

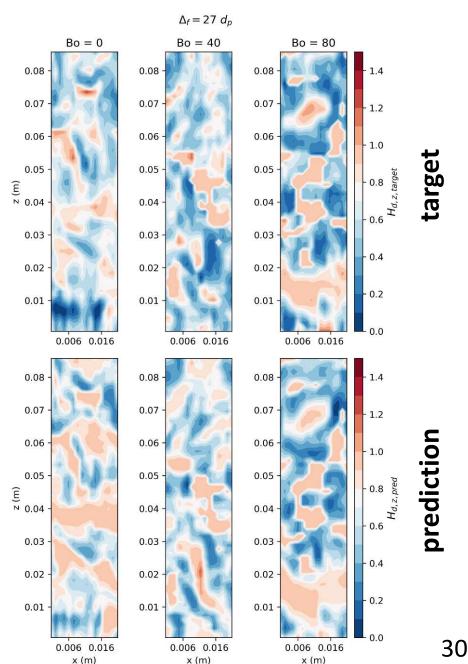


Workflows & ML::Need4Speed::Result V



Graz University of Technology

- 2D & 3D, gravitational direction only
- Spatial distribution of the drag correction functions is sensitive to Bond number ("diffuse" versus "focused" for low and high Bond, respectively)
- Reasonable agreement, except for "extreme" regions (e.g., local maxima in the \boldsymbol{H}_d field)



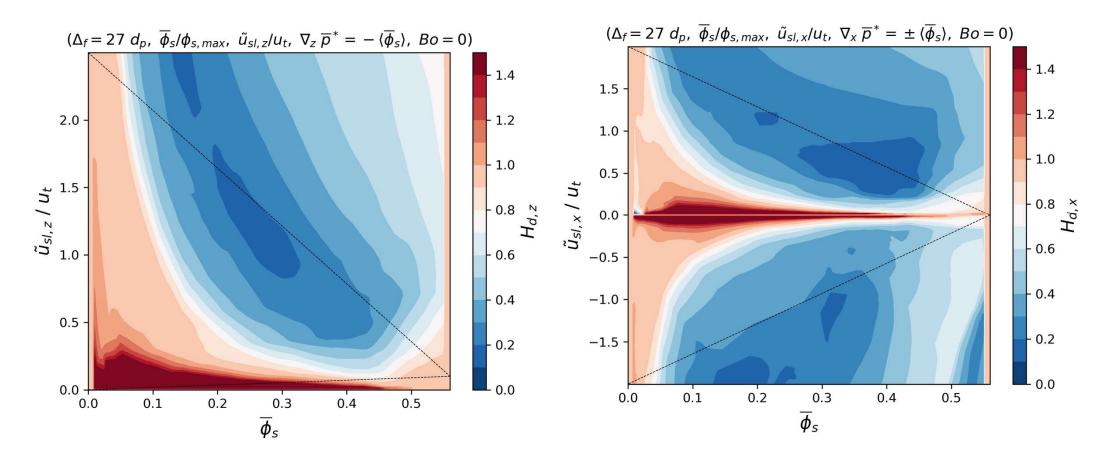
Workflows & ML::Need4Speed::Result VI



• Distribution of correction values in $\overline{\phi}_{\scriptscriptstyle S}$ – $\widetilde{u}_{\scriptscriptstyle Sl}/u_t$ plane

Gravitational direction

Lateral direction

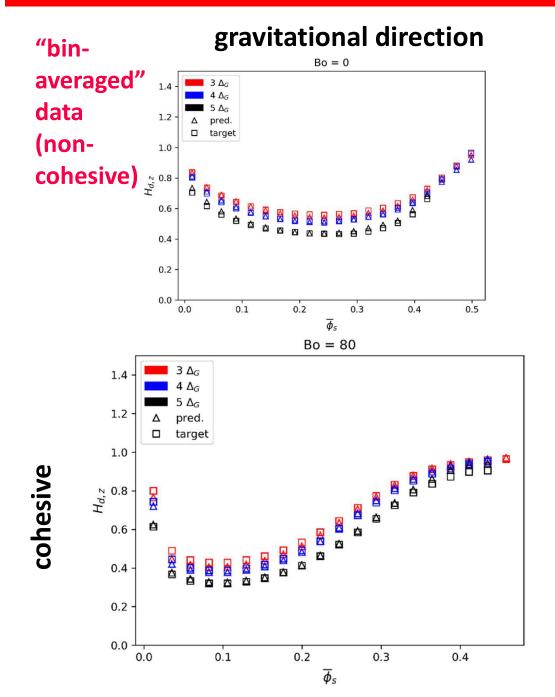


Significant and non-trivial change with Bond number

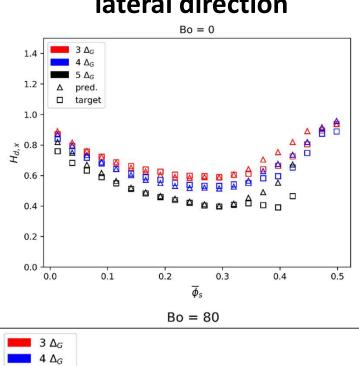
Workflows & ML::Need4Speed::Result VII

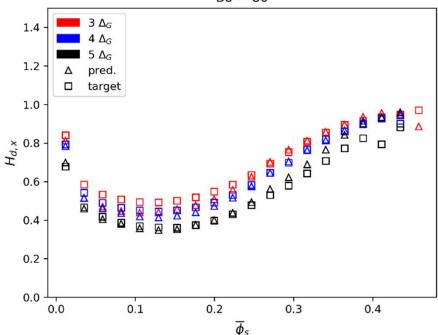


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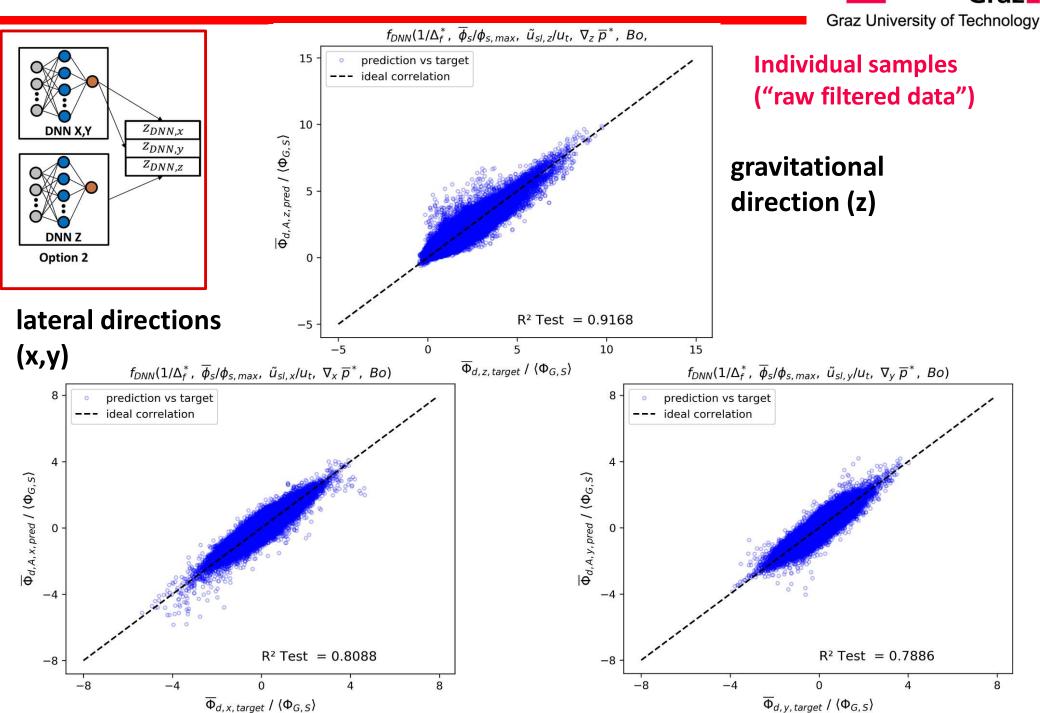
lateral direction





Workflows & ML::Need4Speed::Result VIII







- The "chicken crossing a street challenge": calibration has become a standard approach to make simulations "more realistic"
 - Sequential direct calibration approach (Aspherix® calibration)
 - Response surfaces: Superimposing the results of multiple numerically replicated experiments for a range of parameters

Common challenges

- lack of graphical calibration workflows, or even the workflow
- absence of a clear & FAIR data handling strategy

Irrespective of the calibration method, the workflow needs to handle a huge amount of data

Coetzee, Powder Technology, 2017. Roessler et al, Powder Technology, 2019. Do et al, advanced powder technology, 2018. Richter et al, Powder Technology, 2020



DEMvironment

A workflow environment for data management of DEM parameter calibration process

- Data management
- Guide for experiment selection
- Steers the calibration workflow

- Speeding up the process
- Increase efficiency in model development
- Increased collaboration among researchers and practitioners

Key Features

Benefit

Impact

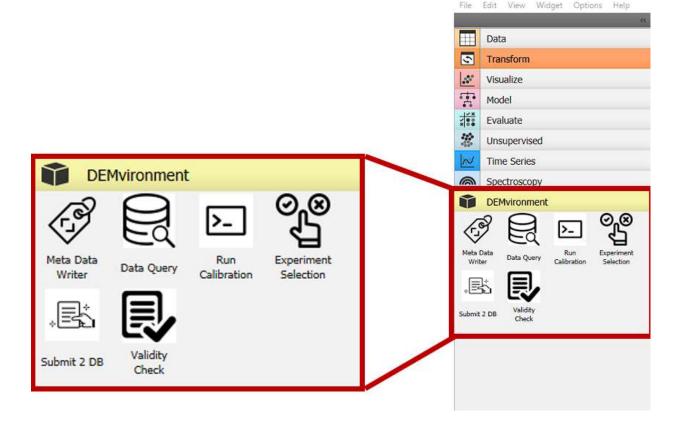
Potentials

- User-friendly interface
- Automated parameter calibration
- Reproducibility of the process
- Open source
- Allows steering more sophisticated ML algorithms
- Can be applied to other particle simulation techniques



DEMvironment interface

...soon available in Orange3







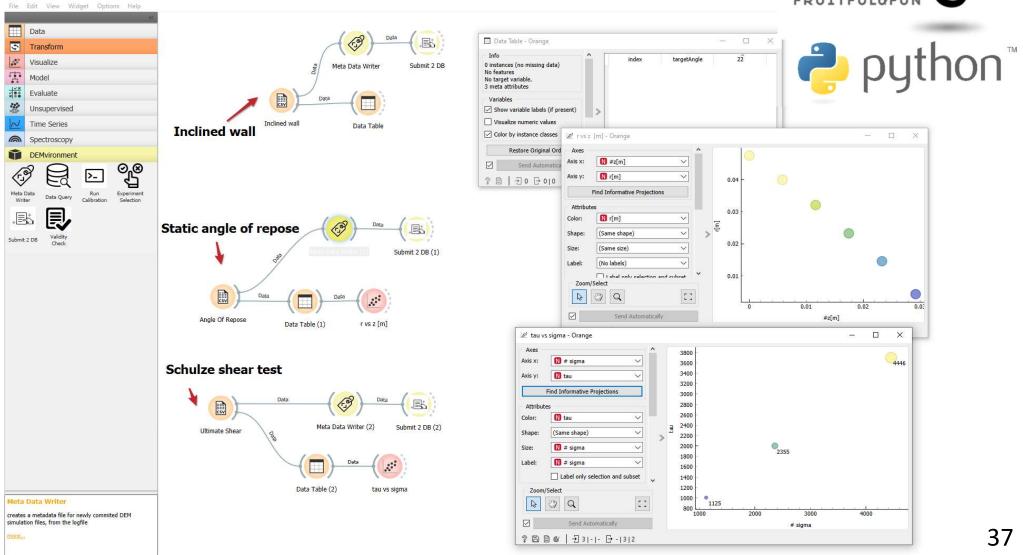
https://n-ghods.github.io/workflowenv



DEMvironment interface

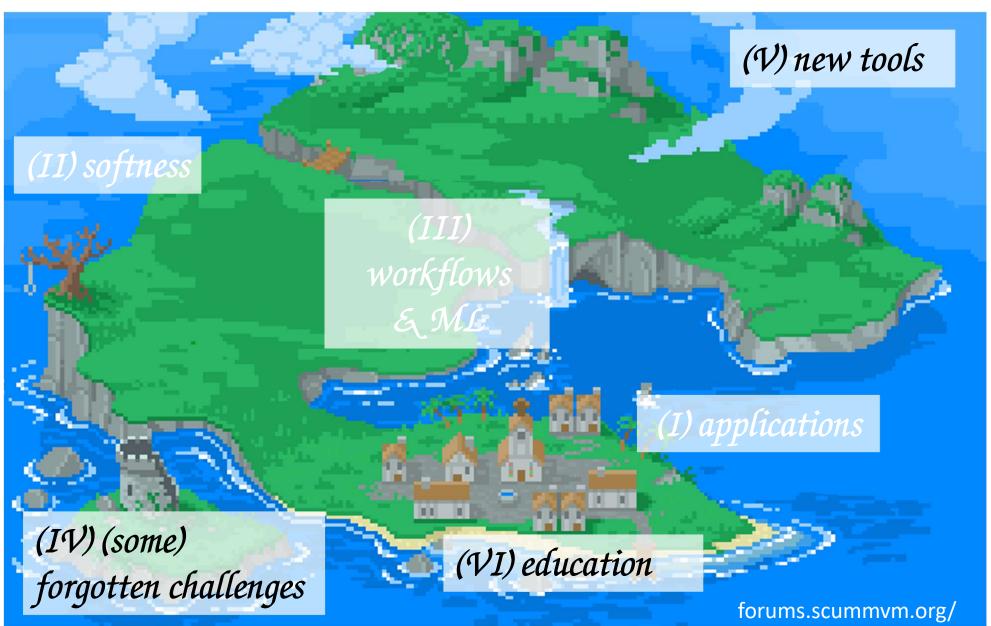
...soon available in Orange3





Overview





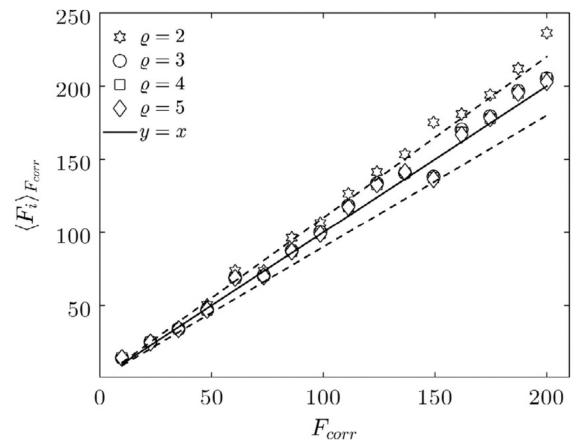
(Some) Forgotten Challenges



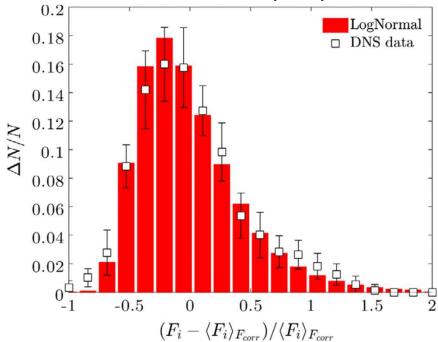
Let us reflect...

What would we need to go "beyond" current CFD-DEM capabilities?

Fluid-particle drag (and Nusselt number) is okay "on average"....



....but there is a wide distribution on a per-particle!



Municchi & Radl, Int J Heat Mass Transfer, 2017

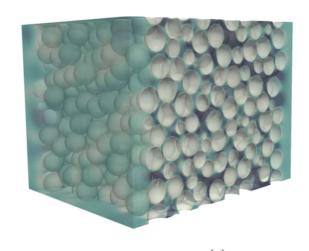
(Some) Forgotten Challenges

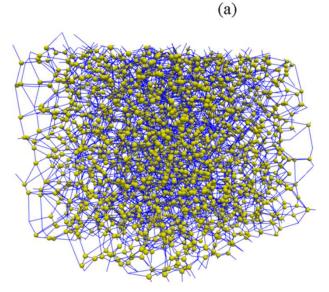


Let us reflect...

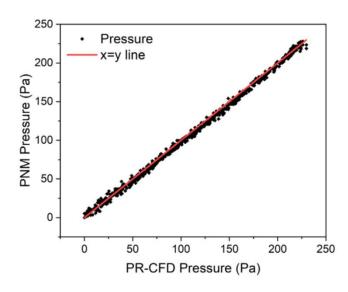
What would we need to go "beyond" current CFD-DEM capabilities?

Possible solution: use a pore network model to improve flow prediction...





....with recent success! But what is the computational cost? Is their calibration universal?



Fathiganjehlou et al., Chem Eng Sci, 2023

Morimoto et al, Computers & Geotechnics, 2022

New Tools



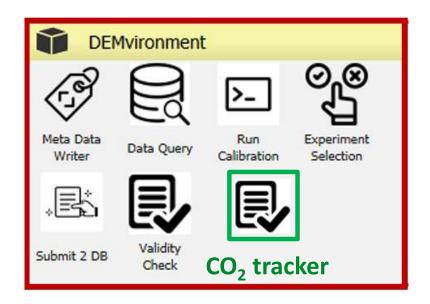
What should happen next...

...tools and their upgrades

- CPPPO's general interface with lagrangian (DEM) data
- Filtering over a fixed number of particles (instead of a fixed region size)
- More filter kernels
- Integration of CO₂ tracker into workflow tool (eco sweet spot of modeling effort)

https://yopad.eu/p/SoSe23_seminarH annover





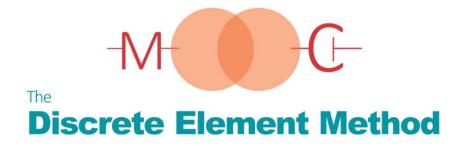
Educational Aspects



- Start slow and simple (analytics first, then simulation; Python first, then C++)
- Use existing tools (Orange3, then KERAS/TensorFlow)
- respect FAIR data management principles (because only complete data is useful data)
- Preservation of knowledge requires a dedicated work package







https://imoox.at/course/dem

MOOC starting in fall 2023

Conclusion I



- Softness must be seen in relative terms (pressure/elasticity ratio)
- Various approaches exist, simple extension to DEM possible (currently only spheres)
- Poisson ratio becomes an additional influence parameter
- Full flexibility (SPH, bonded particles, FEM) comes with significant computational cost
- advanced MC DEM together with calibration a promising strategy



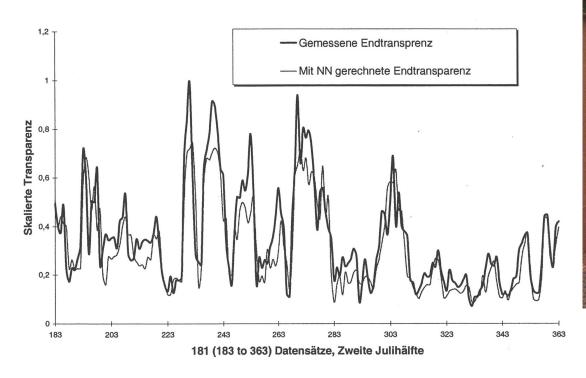




Conclusion II



- (Cohesive) sedimenting suspensions are our daily business since many decades.
 Cohesion may require a paradigm shift to a "closure database" approach
- Reading old PhD thesis can give inspiration for new features to be used in ML (data @ t-∆t, smart NN testing).





Fuchs, Diss. TU Graz, 1999

Conclusion III



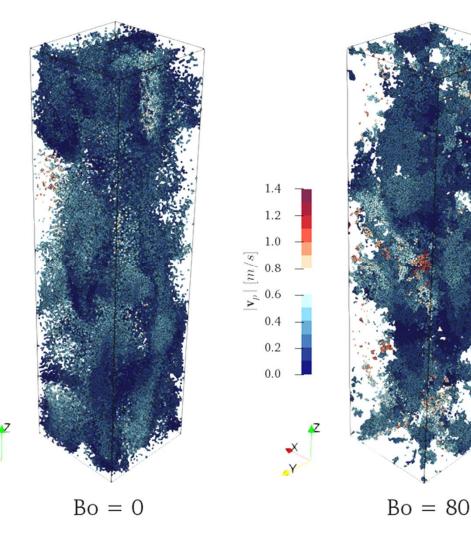
- Anisotropy of drag and stress closures must be considered. "Hand fitting" of this set of 5 marker closures would be extremely time consuming → central motivation for usage of DNNs.
- Huge unexploited potential when considering individual samples of the filtered drag force. Reasons: fundamental assumption $\overline{\Phi}_{d,A} = H_d \ \beta^{Micro} \ \widetilde{u}_{sl}$.
- Drag corrections are stronger (i.e., lower drag forces) for cohesive systems.
 Speculated reason: more compact clusters for high Bo.
- Options for future work
 - DNN-based closure for meso-scale stresses. A posteriori testing of the drag correction models in a fTFM simulation framework
 - "Free" (tabulated, NN-based) force models for coarse graining cohesive powder models



Beyond classical CFD-DEM

Forgotten Challenges and New Tools

Thank you





This project has received funding from the European Union's Horizon 2020 research and innovation programme under the Marie Skłodowska Curie grant agreement No. 812638.

